

$$Y(s) = W(s) U^*(s) = W(s) \sum_{k=0}^{\infty} u(kT) e^{-skT}$$

$$y(t) = \sum_{k=0}^{\infty} w(t-kT) u(kT)$$

↑
siley fr.

$$Y^*(s) = \sum_{n=0}^{\infty} y(nT) e^{-snT} = \sum_{n=0}^{\infty} \left(\sum_{k=0}^{\infty} w([n-k]T) u(kT) \right) e^{-snT}$$

$$Y^*(s) = \sum_{k=0}^{\infty} \sum_{n=k}^{\infty} w(\underbrace{[n-k]T}_i) e^{-s(n-k)T} u(kT) e^{-skT} =$$

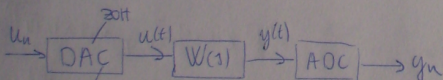
$$= \sum_{k=0}^{\infty} \sum_{i=0}^{\infty} w(iT) e^{-siT} u(kT) e^{-skT} = \left(\sum_{i=0}^{\infty} w(iT) e^{-siT} \right) \left(\sum_{k=0}^{\infty} u(kT) e^{-skT} \right)$$

$$Y^*(s) = W^*(s) U^*(s)$$

$$\sum_{n=0}^{\infty} y(nT) e^{-snT} = \left(\sum_{i=0}^{\infty} w(iT) e^{-siT} \right) \left(\sum_{k=0}^{\infty} u(kT) e^{-skT} \right) \Rightarrow \boxed{z = e^{sT}}$$

Z-Transformiertat Hauptpunkt:

$$\mathcal{Z}\{y(nT)\} = \mathcal{Z}\{w(nT)\} \mathcal{Z}\{u(nT)\} \Rightarrow D(z) = \mathcal{Z}\{w(nT)\}$$



$$\frac{1-e^{-sT}}{s} \Rightarrow W(s) \frac{1-e^{-sT}}{s} = \frac{W(s)}{s} (1-e^{-sT})$$

$$D(z) = (1-z^{-1}) \mathcal{Z}\{x(nT)\}$$

$$W(s) \xrightarrow{z=1} D(z)$$

Ekvivalens átviteli függvény

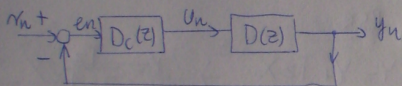
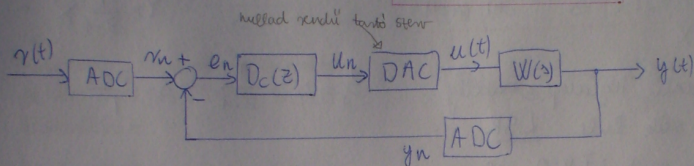
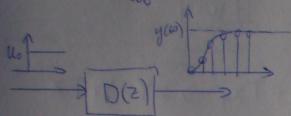
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$$A_{ekv} = \frac{y(\infty)}{u_0}$$

$$Y(z) = D(z) \frac{U_0}{1-z^{-1}}$$

$$y(\infty) = \lim_{z \rightarrow 1} (1-z^{-1}) Y(z) = D(1) u_0$$

$$A_{ekv} = \frac{y(\infty)}{u_0} = D(1)$$



$$D_{gr} = \frac{D_c D}{1 + \underbrace{D_c D}_{D_0}}$$

$$D_{ur} = \frac{D_c}{1 + \underbrace{D_c D}_{D_0}}$$

$$D_0(z) = D_c(z) D(z) \text{ felnyitott kör}$$

Stabilitás vizsgálata

1) Analóg stabilitás mintavetelés közelítése

ω_c, T (analóg)

$T = ?$

$$\frac{\omega_c T}{2} = 5^\circ \frac{\pi}{180} \Rightarrow \omega_c T = \frac{10\pi}{180} = \frac{\pi}{18} = 0.17$$

$$\underline{\omega_c T \approx 0.2}$$

Közelítések: $\frac{d}{dt} \Leftrightarrow s$, $\int dt \Leftrightarrow \frac{1}{s} = s^{-1}$

1) $\frac{dy}{dt} \rightarrow sY$

$$\frac{dy}{dt} = \frac{y(t) - y(t-T)}{T} \rightarrow \frac{1}{T} (Y - z^{-1}Y) = \frac{1-z^{-1}}{T} Y$$

$$s \approx \frac{1-z^{-1}}{T} = \frac{z-1}{Tz}$$

hátraható differencia

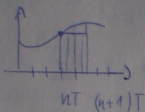
BWD

back ward diff.

$$\frac{dy}{dt} \approx \frac{y(t+T) - y(t)}{T} \rightarrow \frac{zY - Y}{T} = \frac{z-1}{T} Y$$

$\approx \frac{z-1}{T}$ előzetes diff. forward diff. FWD

$$\textcircled{2} y(t) = \int_0^t x(\tau) d\tau$$



$$y_{n+1} = y_n + T x_n \rightarrow zY = Y + TX$$

$$Y = \frac{T}{z-1} X$$

$$Y = \frac{1}{z} X$$

Baloldali félalap stabilis
left side Rule LSR

$$\frac{1}{z} = z^{-1} = \frac{T}{z-1} \rightarrow z = \frac{z-1}{T}$$

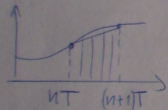
Megegyezik: FWD-vel

$\textcircled{4}$ Jobb oldali félalap stabilis RSR

$$y_{n+1} = y_n + T x_{n+1} \Rightarrow zY = Y + TzX \quad ; \quad Y = \frac{Tz}{z-1} X$$

$$\frac{1}{z} = z^{-1} = \frac{Tz}{z-1} \rightarrow z = \frac{z-1}{Tz}$$

$\textcircled{5}$ Trapéz stabilis, Tustin - képlet



$$y_{n+1} = y_n + \frac{x_n + x_{n+1}}{2} T$$

$$zY = Y + \frac{T}{2}(X + zX)$$

$$Y = \frac{T}{2} \frac{z+1}{z-1} X$$

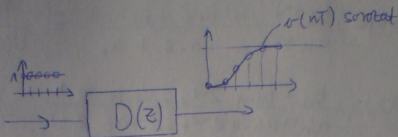
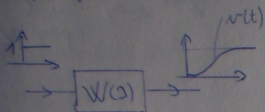
$$\frac{1}{z} = z^{-1} = \frac{T}{2} \frac{z+1}{z-1} \rightarrow z = \frac{z-1}{z+1} \text{ Tustin képlet}$$

Átkalás: $W_c(s) \rightarrow D_c(z)$
 \rightarrow közelítés

Közeliések helyett alkalmazhatunk ekvivalenciákat is!

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Egyesügrás ekvivalencia



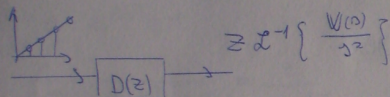
$$Z\{v(nT)\} = D(z) \frac{1}{1-z^{-1}}$$

$$D(z) = (1-z^{-1}) Z\{v(nT)\}$$

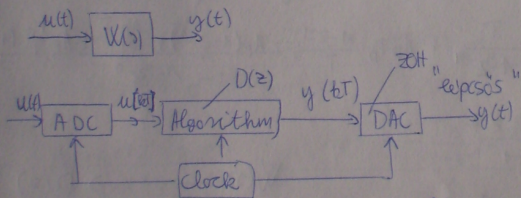
↑
Ezt már egyetemes kiismoltuk de épp most is ez a legegyszerűbb használatos.

$$W(s) \xrightarrow[\text{'Zoh'}]{\text{C2D}} D(z)$$

Sebességűgrás ekvivalencia



$$Z\{v(nT)\} = D(z) \frac{Tz^{-1}}{(1-z^{-1})^2} \rightarrow D(z) = \frac{(1-z^{-1})^2}{Tz^{-1}} Z\{v(nT)\}$$



$$\tilde{W}(j\omega) = \frac{1-e^{-j\omega T}}{j\omega} D(z=e^{j\omega T})$$

Approximáció juttal:

Javulási sémák:

Tusti
egységnyi ekv.
sebességű ekv. ↓ javul.

Algorithm:

$$D(z) = \frac{b_n z^n + \dots + b_1 z + b_0}{a_n z^n + \dots + a_1 z + a_0} = \frac{Y(z)}{U(z)} \quad z^{-k} \leftrightarrow \text{shift operator}$$

$$D(z) = \frac{b_n + b_{n-1} z^{-1} + \dots + b_0 z^{-n}}{a_n + a_{n-1} z^{-1} + \dots + a_0 z^{-n}} = \frac{Y(z)}{U(z)}$$

$$a_n y_k + a_{n-1} y_{k-1} + \dots + a_0 y_{k-n} = b_n u_k + b_{n-1} u_{k-1} + \dots + b_0 u_{k-n}$$

$$y_k = -\frac{a_{n-1}}{a_n} y_{k-1} - \dots - \frac{a_0}{a_n} y_{k-n} + \frac{b_n}{a_n} u_k + \dots + \frac{b_0}{a_n} u_{k-n}$$

$$\{y_{k-1}, y_{k-2}, \dots, y_{k-n}, u_k, u_{k-1}, \dots, u_{k-n}\} \rightarrow y_k$$

ALGORITHM

Analóg PID mintavetelés készítése

① Ideális PID

$$W_{PID}(s) = A_P \left(1 + \frac{1}{sT_I} + sT_D \right) = A_P + \frac{A_P}{T_I} \frac{1}{s} + A_P T_D s$$

$$\text{Készítés: BWD = RSR} \quad s = \frac{z-1}{T} = \frac{1-z^{-1}}{T}$$

$$D_{PID}(z) = A_P + \frac{A_P}{T_I} \frac{T}{1-z^{-1}} + A_P T_D \frac{1-z^{-1}}{T} = \frac{A_P(1-z^{-1}) + \frac{A_P T}{T_I} + A_P \frac{T_D}{T} (1-z^{-1})^2}{1-z^{-1}}$$

$$= \frac{q_0 + q_1 z^{-1} + q_2 z^{-2}}{1-z^{-1}}$$

$$q_0 = A_P \left\{ 1 + \frac{T}{T_I} + \frac{T_D}{T} \right\}$$

$$q_1 = -A_P \left\{ 1 + \frac{2T_D}{T} \right\}$$

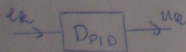
$$q_2 = A_P \frac{T_D}{T}$$

$$W(s) \longrightarrow D(z)$$

$z^i = e^{s_i T}$ helyre beépítve a pólusok

integrátor esetén:

$$s_i = 0 \longrightarrow z_i = 1$$



② Kézeltető PID

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G.h.

$$W_{PID}(s) = A_p \left(1 + \frac{1}{sT_I} + \frac{sT_D}{1+sT_C} \right) = A_p + \frac{A_p}{T_I} \frac{1}{s} + \frac{A_p T_D}{T_C} \frac{1}{s + \frac{1}{T_C}}$$

Egységyenlő alak:

$$w_{PID}(t) = \mathcal{L}^{-1} \left\{ \frac{A_p}{s} + \frac{A_p}{T_I} \frac{1}{s^2} + \frac{A_p T_D}{T_C} \frac{1}{s + \frac{1}{T_C}} \right\} = A_p + \frac{A_p}{T_I} t + \frac{A_p T_D}{T_C} e^{-\frac{t}{T_C}}, \quad t \geq 0$$

$$D_{PID}(z) = (1-z^{-1})z \{ r_{PID}(nT) \} = (1-z^{-1}) \left\{ A_p \frac{1}{1-z^{-1}} + \frac{A_p}{T_I} \frac{Tz^{-1}}{(1-z^{-1})^2} + \frac{A_p T_D}{T_C} \frac{1-z^{-1}}{1-e^{-T/T_C} z^{-1}} \right\}$$

$$e^{sT} \rightarrow \{ 1 + e^{sT} z^{-1} + e^{2sT} z^{-2} + \dots \}$$

$$q = e^{sT} z^{-1}$$

$$\frac{1}{1-q} = \frac{1}{1-e^{sT} z^{-1}} = \frac{z}{z-e^{sT}}$$

Matlab

$$D_{PID}(z) = A_p + A_p \frac{T_D}{T_C} \frac{z^{-1}}{1-z^{-1}} + \frac{A_p T_D}{T_C} \frac{1-z^{-1}}{1-e^{-T/T_C} z^{-1}} =$$

$$= \frac{A_p(1-z^{-1})(1-e^{-T/T_C} z^{-1}) + \frac{A_p}{T_I} T z^{-1} (1-e^{-T/T_C}) z^{-1} + \frac{A_p T_D}{T_C} (1-z^{-1})^2}{(1-z^{-1})(1-e^{-T/T_C} z^{-1})}$$

$$D_{PID}(z) = \frac{q_0 + q_1 z^{-1} + q_2 z^{-2}}{p_0 + p_1 z^{-1} + p_2 z^{-2}} = \frac{A_p + \frac{A_p T z^{-1}}{T_I} + \frac{A_p T_D}{T_C} \frac{1-z^{-1}}{1-e^{-T/T_C} z^{-1}}}{1}$$

$$p_0 = 1$$

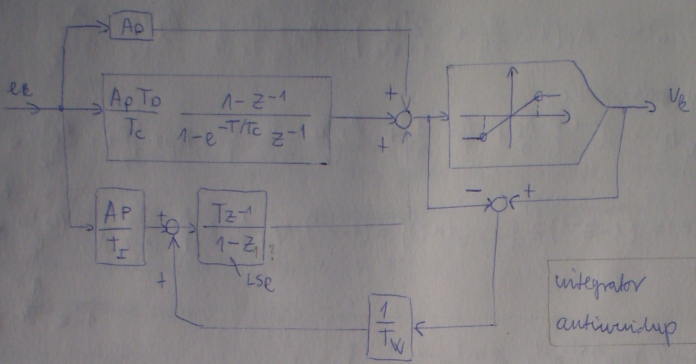
$$p_1 = -(1 + e^{-T/T_C})$$

$$p_2 = e^{-T/T_C}$$

$$q_0 = A_p \left\{ 1 + \frac{T_D}{T_C} \right\}$$

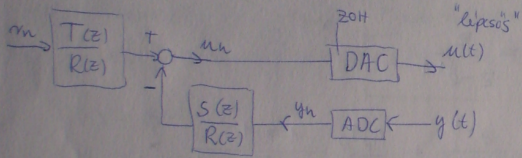
$$q_1 = -A_p \left\{ 1 + e^{-T/T_C} - \frac{T}{T_I} + \frac{2T_D}{T_C} \right\}$$

$$q_2 = A_p \left\{ e^{-T/T_C} \left(1 - \frac{T}{T_I} \right) + \frac{T_D}{T_C} \right\}$$

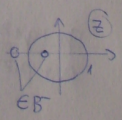
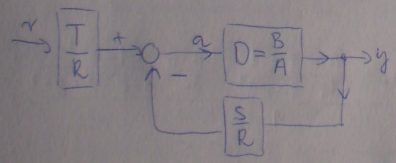
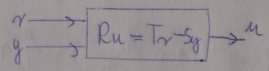


integrator
antiműködés

2 szabványosított stabilitási : 2-DOF



$$u = \frac{T}{R} r - \frac{S}{R} y \Leftrightarrow Ru = Tr - Sy$$



$$\frac{\frac{T}{R} \frac{B}{A}}{1 + \frac{S}{R} + \frac{B}{A}} = \frac{TB}{AR + BS} = \frac{B_m}{A_m} \cdot \frac{A_o}{A_o}$$

$$B = B^+ B^-$$

B⁻: „egységkörön kívüli”
Zérusok helyét

• valósak, de -1-es 0
között foglalnuk kell

$$R = B^+ R^- = B^+ (z-1)^l R_1$$

integrálból
db száma

$$-a = e^{sT} \rightarrow s_i = \frac{1}{T} \ln(-a)$$

$$\frac{T B^+ B^-}{A B^+ (z-1)^l R_1^+ + B^+ B^- S} = \frac{B^- B_m^+}{A_m} \frac{A_0}{A_0}$$

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$A_0 =$ megfigyelő polinom

$$B_m = B^- B_m^+$$

$$T = B_m A_0$$

$$A (z-1)^l R_1^+ + B^- S = A_m A_0$$

Ez egy polinom egyenlet, megoldható
"diophantosei" ("diophantosei")

1- uszto együttható: A_m, A_0, A, B^+, R_1^+

l : integrátorok száma (0, 1, 2)

azaz monik

Nem monik: T, S

gr (fokszám):

T -nek a fokszáma

$$\textcircled{1} \frac{T}{R} \text{ és } \frac{S}{R} \text{ kauzális} \Leftrightarrow \text{gr}(T) \leq \text{gr}(R), \text{ gr}(S) \leq \text{gr}(R)$$

$$\textcircled{2} AX + BY = C$$

$$X_0, Y_0 \text{ megoldás} \Rightarrow X_0 + QB, Y_0 - QA$$

$$A(X_0 + QB) + B(Y_0 - QA) = AX_0 + BY_0 + AQB - BQA = C$$

Egyetlen megoldás van, ha $\text{gr}(X) < \text{gr}(B)$ és $\text{gr}(Y) < \text{gr}(A)$

③ Eredő fokszám feltételek:

$$\text{gr}(A_m) - \text{gr}(B_m) \geq \text{gr}(A) - \text{gr}(B)$$

$$\text{gr}(S) = \text{gr}(A) + l - 1$$

$$\text{gr}(A_0) \geq 2\text{gr}(A) + l - 1 - \text{gr}(B^+) - \text{gr}(A_m)$$

$$\text{gr}(R_1^+) = \text{gr}(A_m) + \text{gr}(A_0) - \text{gr}(A) - l$$

$$AX + BY = C$$

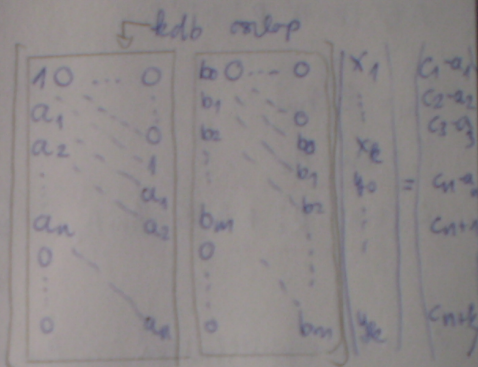
$$A = z^n + a_1 z^{n-1} + \dots + a_n$$

$$B = b_0 z^m + b_1 z^{m-1} + \dots + b_m$$

$$X = z^k + x_1 z^{k-1} + \dots + x_l$$

$$Y = y_0 z^k + y_1 z^{k-1} + \dots + y_n$$

$$C = z^{n+k} + c_1 z^{n+k-1} + \dots + c_{n+k}$$



Háttér:

$$A := A(z-1)^l$$

$$B := B^-$$

$$X := R_1'$$

$$Y := S$$

$$C := A_m A_0$$