

## A CSOPORT

①

1.) Az integrátor bevezetése  $e=0$ .

$$\tau = 3y^2 + 4$$

$$\text{Tehát } y = \sqrt{\frac{\tau - 4}{3}}$$

2.)  $\tau > T$  esetén a rendszer stabilis.  
 $\tau < T$  esetén a rendszer labilis.

Indoklás

A kar. egyenlet:

$$1 + L(s) = 1 + \frac{1+sT}{s^2(1+sT)} = 0$$

$$s^3T + s^2 + sT + 1 = 0$$

Hurwitz det.:

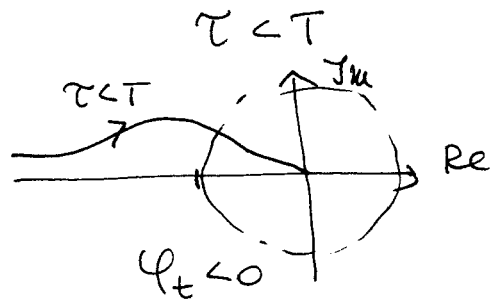
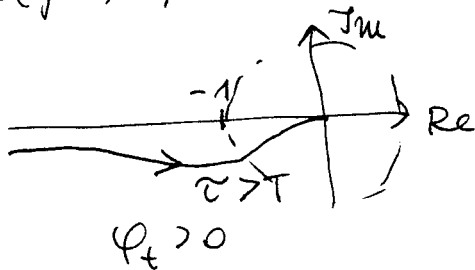
$$\begin{vmatrix} 1 & 1 & 0 \\ T & -T & 0 \\ 0 & 1 & 1 \end{vmatrix}$$

$$\Delta_2 = \tau - T > 0$$

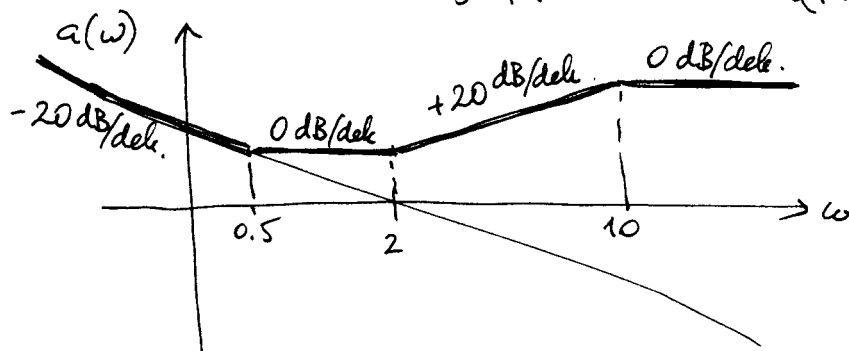
Stab. feltétele  $\tau > T$

Vagy a Nyquist stab. kritérium alapján:

$L(j\omega)$ , ha  $\tau > T$



$$3.) L(s) = 20 \frac{s^2 + 2.5s + 1}{s^2 + 10s} = \frac{2(s+2)(s+0.5)}{s(1+0.1s)} = \frac{2(1+0.5s)(1+2s)}{s(1+0.1s)}$$



1. ZH MEGOLDÁSOK, A CSOPORT, 1. folyt. (2)

4.)  $L(s) = \frac{1}{s(1+s)^2}$  ;  $L(j\omega) = \frac{1}{j\omega(1+j\omega)^2}$

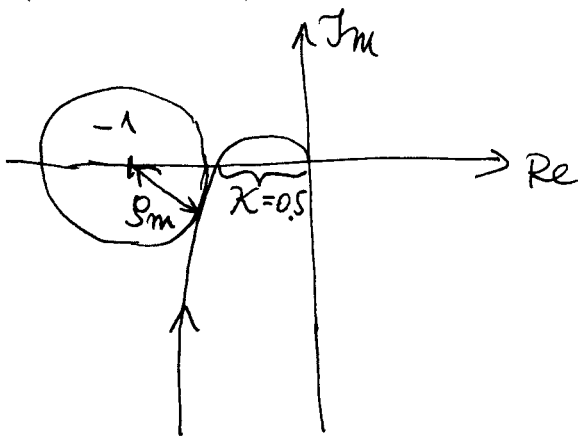
$\varphi = -180^\circ$ , ha

$-90^\circ - 2 \arctg \omega_0 = -180^\circ$ .

$\arctg \omega_0 = 45^\circ \Rightarrow \omega_0 = 1$ .

$|L(j\omega_0)| = \frac{1}{\omega_0(\sqrt{1+\omega_0^2})^2} = \frac{1}{1 \cdot 2} = 0.5$

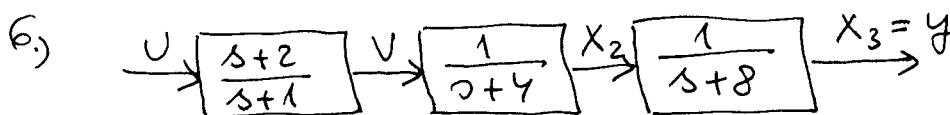
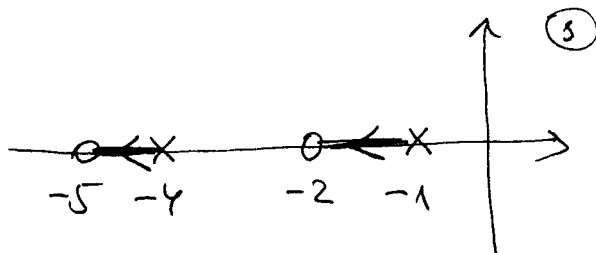
Tehát a Nyquist diagramtól a  $-1+j0$  pont balra felé esik, tehát a rendszer stabilis.



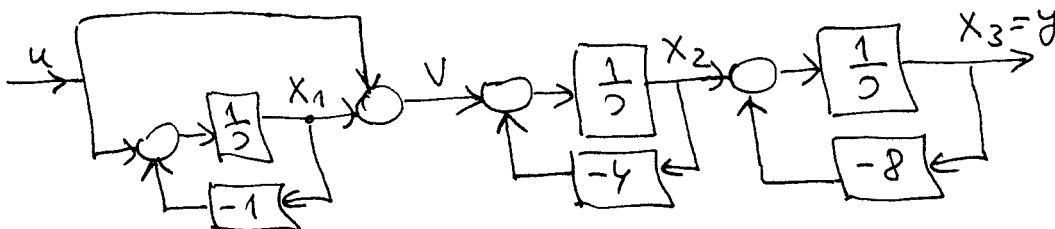
Erőnövelési tartomány:  $1/K = \frac{1}{0.5} = 2$

5.) A gyökélgörbe a zárt <sup>rendszer</sup> karakterisztikus egyenletének gyökeit adja meg miközben valamelyik paraméter (rendszerint a hurokátényező (körerőnövelés)) 0 és  $\infty$  között változik.

$L(s) = K \frac{s^2 + 7s + 10}{s^2 + 5s + 4} = K \frac{(s+2)(s+5)}{(s+1)(s+4)}$



ill.



$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \underbrace{\begin{bmatrix} -1 & 0 & 0 \\ 1 & -4 & 0 \\ 0 & 1 & -8 \end{bmatrix}}_A \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \underbrace{\begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix}}_b u$$

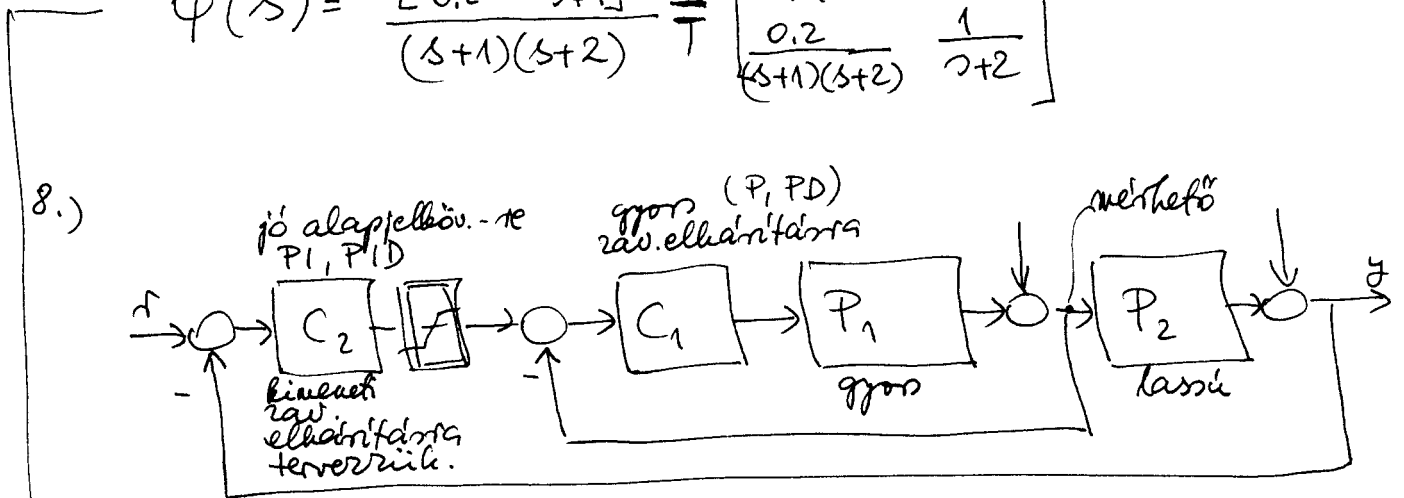
$$y = \underbrace{[0 \quad 0 \quad 1]}_{c^T} X + \underbrace{0}_{d} \cdot u$$

A statikus erőrités:  $\frac{2 \cdot 1}{1 \cdot 4 \cdot 8} = \frac{1}{16}$

7.)  $\phi(t) = e^{At} = e^{\begin{bmatrix} -1 & 0 \\ 0.2 & -2 \end{bmatrix} t} = \mathcal{L}^{-1}[\phi(s)] = \mathcal{L}^{-1}[(sI - A)^{-1}]$

$$X(1) = e^{A \cdot 1} X(0) = e^{At} \cdot \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$\phi(s) = \frac{\begin{bmatrix} s+2 & 0 \\ 0.2 & s+1 \end{bmatrix}}{(s+1)(s+2)} = \begin{bmatrix} \frac{1}{s+1} & 0 \\ \frac{0.2}{(s+1)(s+2)} & \frac{1}{s+2} \end{bmatrix}$$

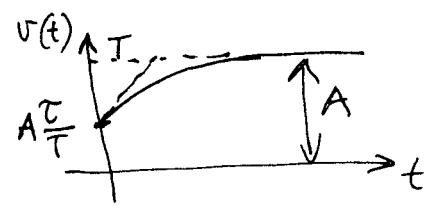


$$\phi(t) = \begin{bmatrix} e^{-t} & 0 \\ 0.2e^{-t} - 0.2e^{-2t} & e^{-2t} \end{bmatrix}$$

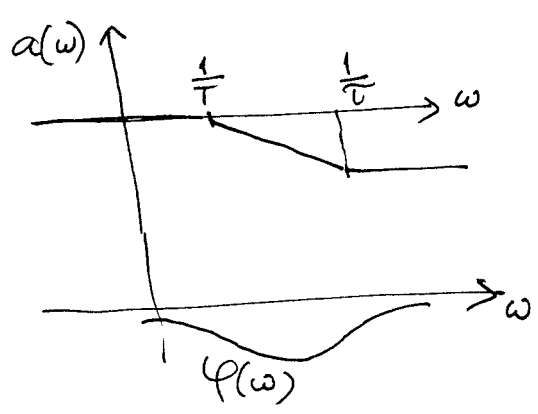
$$x_1(1) = e^{-1} \cdot 1$$

1.)  $H(s) = A \frac{1+sT}{1+sT}$

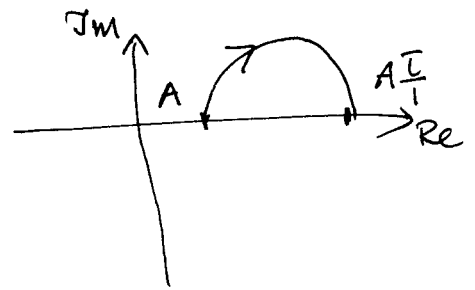
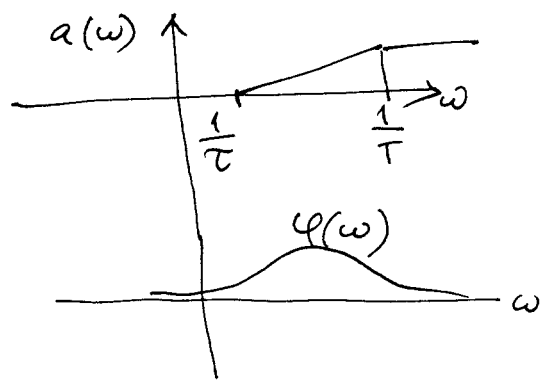
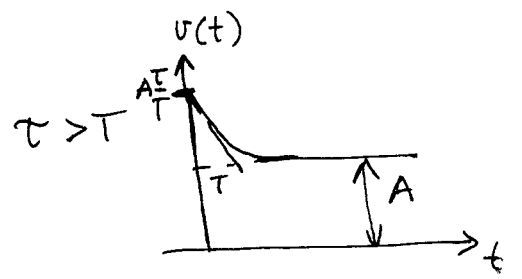
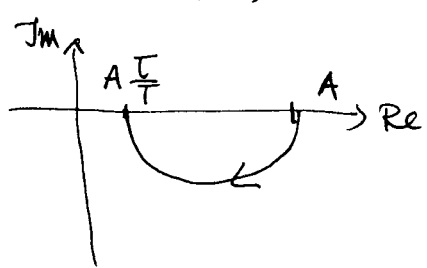
$\tau < T$



Bode:



Nyquist:



2.)  $P(s) = \frac{5 e^{-0.5s}}{(1+s)(1+2s)(1+3s)}$

$a(\omega) = \frac{5}{\sqrt{1+\omega^2} \cdot \sqrt{1+4\omega^2} \cdot \sqrt{1+9\omega^2}}$

$\varphi(\omega) = -0.5\omega \cdot 180/\pi - \arctg \omega - \arctg 2\omega - \arctg 3\omega$

3.)  $L(s) = \frac{K}{(1+s)^3}$

Hurwitz det.:

Kar. egyenlet:

$1 + \frac{K}{(1+s)^3} = 0$

$$\begin{vmatrix} 3 & 1+K & 0 \\ 1 & 3 & 0 \\ 0 & 3 & 1+K \end{vmatrix}$$

$s^3 + 3s^2 + 3s + 1+K = 0$

$\Delta_2 = 9 - 1 - K > 0$

$K < 8$

vagy a Nyquist stab. krit. alapján:

1. ZH MEGOLDÁSOK, B CSOPORT 1. főljt.

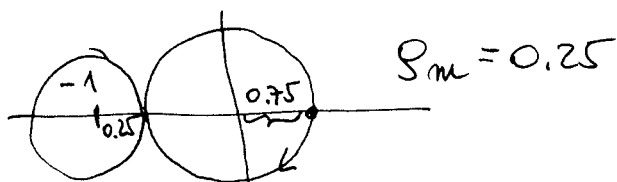
(2)

$$\varphi(\omega_0) = -3 \arctg \omega_0 = -180^\circ ; \arctg \omega_0 = 60^\circ$$

ahol  $-180^\circ$  a fázisrög  $\omega_0 = \sqrt{3}$

$$|L(j\omega_0)| = \frac{K_{kr}}{(\sqrt{1+\omega_0^2})^3} = 1 ; K_{kr} = (\sqrt{1+3})^3 = 8$$

4.) A modulus tartalek a  $-1+j0$  pont ~~és~~ köreppontú, a felnyitott kör Nyquist diagramját érintő kör sugara.  $L(j\omega) = 0.75e^{-3j\omega}$



5.)

$$|P(j3)| = \frac{5}{\sqrt{1+9}}$$

$$\varphi(\omega=3) = -\arctg 3 - 0.2 \cdot 3 \cdot 180/\pi$$

$$y_{stac} = \frac{5}{\sqrt{10}} \sin(3t - \varphi)$$

6.)

$$\phi(t) = e^{At} ; \phi(s) = (sI - A)^{-1}$$

$$\phi(s) = \begin{bmatrix} s+1 & 0 \\ -0.2 & s+2 \end{bmatrix}^{-1} = \frac{\begin{bmatrix} s+2 & 0 \\ 0.2 & s+1 \end{bmatrix}}{(s+1)(s+2)} = \begin{bmatrix} \frac{1}{s+1} & 0 \\ \frac{0.2}{(s+1)(s+2)} & \frac{1}{s+2} \end{bmatrix}$$

$$\phi(t) = \begin{bmatrix} e^{-t} & 0 \\ 0.2e^{-t} - 0.2e^{-2t} & e^{-2t} \end{bmatrix}$$

$$x_2(1) = 0.2e^{-1} - 0.2e^{-2} + e^{-2} = 0.2e^{-1} + 0.8e^{-2}$$

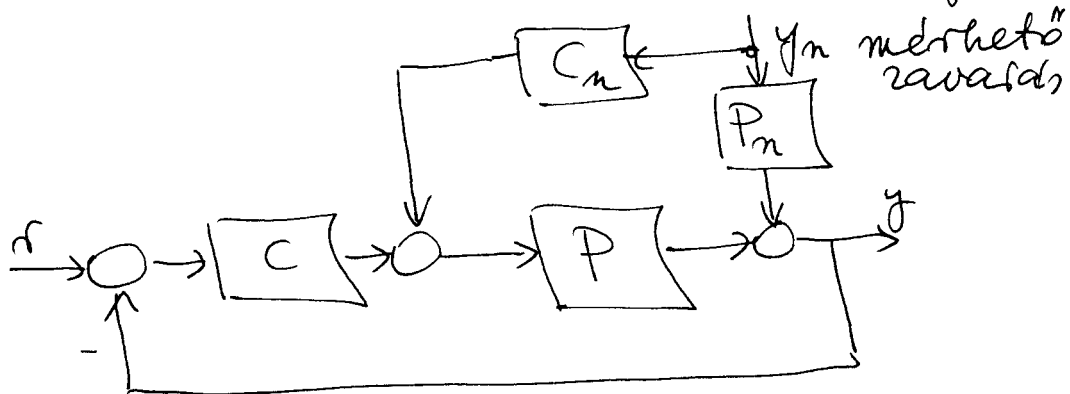
$$7.) \quad T = \frac{CP}{1+CP}$$

$$\Delta T = \frac{\partial T}{\partial P} \Delta P = \frac{C}{(1+CP)^2} \Delta P$$

$$\frac{\Delta T}{T} = \frac{1}{1+CP} \frac{\Delta P}{P} = S \frac{\Delta P}{P}, \quad \text{ahol } S = \frac{1}{1+CP}$$

az érzékenységi fű.

8.)



A zavarcompenzáció alkalmazható mérhető zavarás esetén. Előrecsatolás a zavarásról.

Ideális, ha

$$y_n \left( \frac{P_n}{1+CP} + \frac{C_n P}{1+CP} \right) = 0$$

$$\text{Tehát } P_n + C_n P = 0$$

$$C_n = - \frac{P_n}{P}$$

Akkor realizálható, ha a nevező fokszáma  $\geq$  számláló fokszáma.

A holtidő nem kompenzálható.